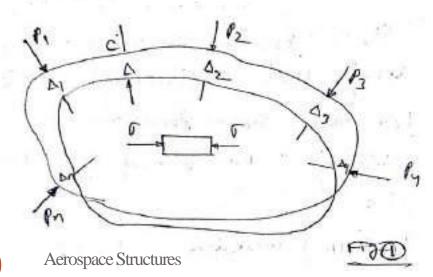
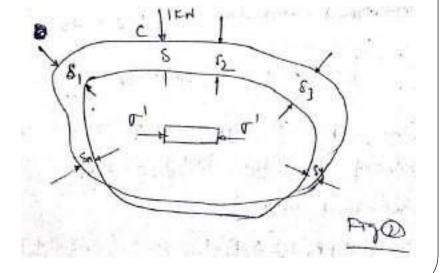
	Unit Lo	oad Me	thod	
Aerospace Struc	ctures			

Proof of Unit Load Method

Consider the body shown in fig. which is subjected to forces P1, P2, P3, P4... In applied gradually. Let the displacement under load points be A1, A2, A3... An and at point.

 $C \sim \Delta$.





and stain emergy streed = It de e dr. more T= stack e = stoain in the element. . External work dore = strain enougy store of 2 AIPI + 2 A1P2 + 2 A3B+ - + 2 AnPn = 120.edv 10 March 1990 Now, Consider the same body subjected to an unit local applied gradually at c when it is free of system of p'force) let the displacements at 1,2,3... n be SI, S2, S3, ... Son respectively and the displacement of it be's? let the stock produced in the element be I and the strain. be e'

External workdore = 1×1×5. 10/ternel workdore = Storedv. ±xixs = j± d'el.dv -Dow, if P'system of forces 13 applied to the body of main infig@ 62 nd erned work den Since, unit load 3 already acting.

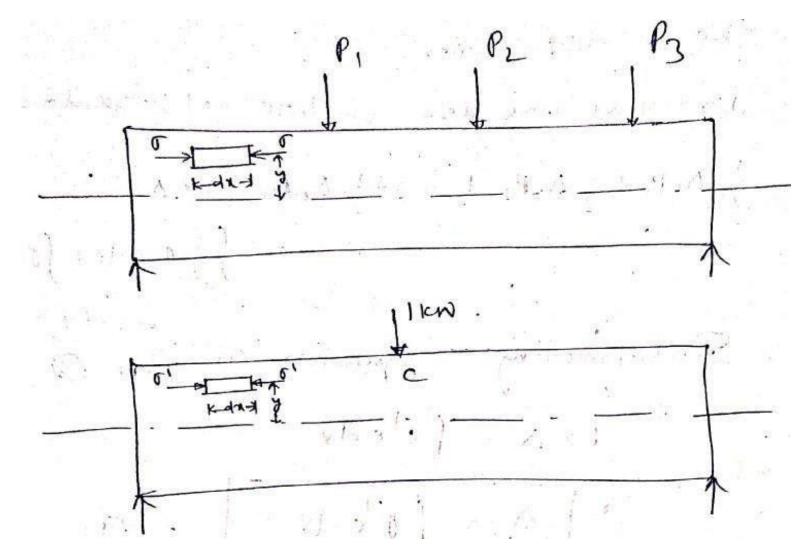
Since the stock of its acting throughout the deformation.

External work dore = Internal work done

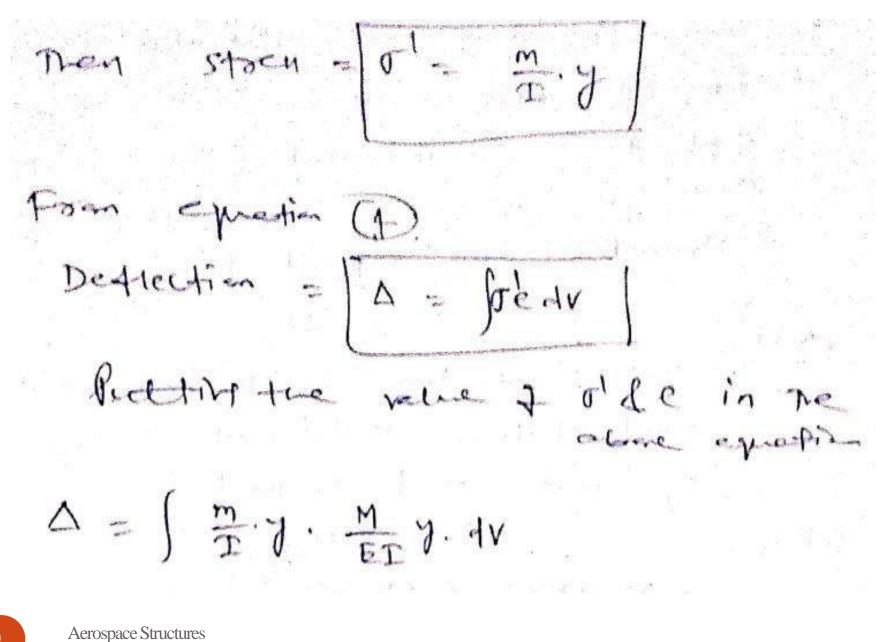
- Δ1P1+ + Δ2P2+···+ ΔnPn+1×Δ = Storedr + Soledr. Subtracting equation O from O 1×A - foredy s. | △ = J fedv

flection at foint where applied Local TS and 15 measured in the direction of whit had Stren in element an due 1-10. unit long Strain lement in e due to given Load System

Application of Unit Load Method to Beam Deflection



beam Subjected Consider th to a system of p' force clement et a in the The stocu distance from neutral axis is 9 C= My inere M = Moment acting at the section due to given the element Storin in system of force Is = M EI J m the moment at 13 with local acting at ic Section due to



$$\Delta = \int \frac{m}{ET} M_{T} \cdot J^{T} dV$$

$$= \int \frac{m}{ET} M_{T} \left(\int J^{T} dA \right) dX$$

$$R_{n+1} \left(\int J^{T} dA - T \right)$$

$$R_{n+1} \left(\int J^{T} dA - T \right)$$

$$\Delta = \int \frac{M}{ET} M_{T} \cdot T \cdot dX$$

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$$\Delta = \int \frac{M}{ET} dX$$

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$$\Delta = \int M_{T} \cdot T \cdot dX$$

Procedure 73 applicatione o sidis Thes frame) also, where may flexure extect Constalered (ie ir analysis in which the effect 2 ana) f-shear forces neplected) are

Deflection by Unit Load Method

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Deflection by Unit Load Method

- This method is applicable to beam and rigid frame where only flexural effect is considered.
- In the analysis, the effect of axial force and shear forces are neglected.
- The deflection at any point can be find out by:

$$= \int_{0}^{L} \frac{Mm}{EI} dx$$

Where, M = Bending moment at the section due to the external forces m = Bending moment at the section due to unit loading E = Modulus of Elasticity I = Moment of Inertia of the section Q1. Determine the deflection at the free end of the over hanging beam shown in Figure by unit load method.

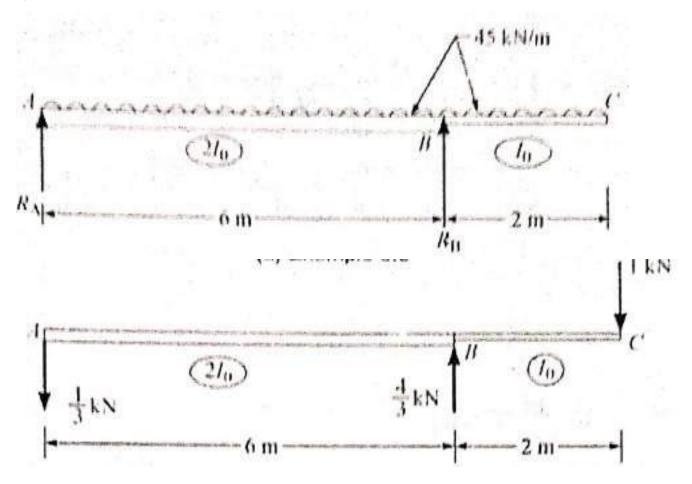


Figure 1: Beam with unit load at 'C'

• Find out the reactions due to external forces, taking moment about A

$$\Sigma M_{\Lambda} = 0, \text{ gives}$$

$$R_{B} \times 6 = 45 \times 8 \times 4$$

$$R_{B} \approx 240 \text{ kN}$$

$$\Sigma V = 0, \text{ gives}$$

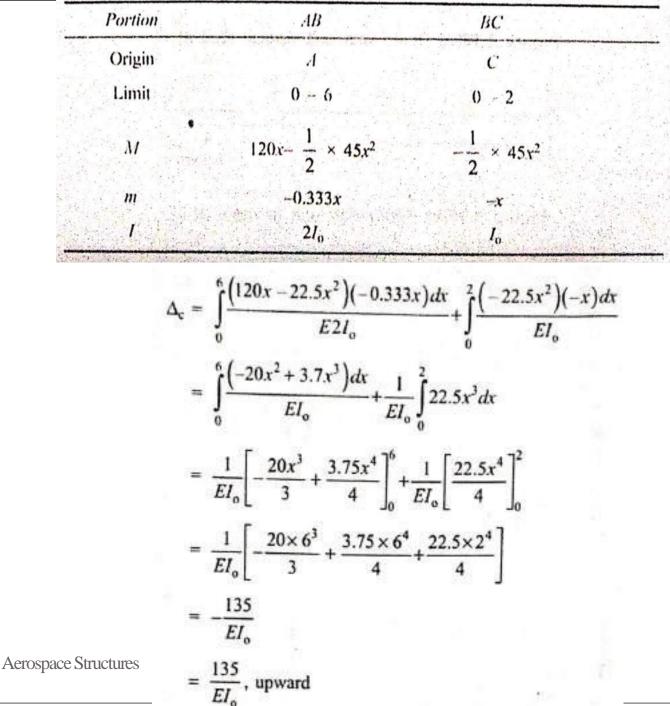
$$R_{\Lambda} = 45 \times 8 - 240 = 120 \text{ kN}$$

• Find out the reactions, when unit load acting at 'C'

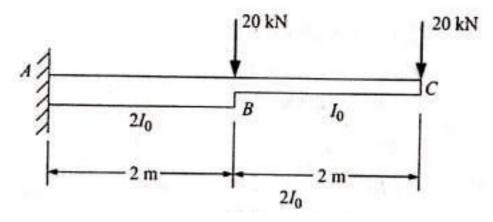
$$R_{\rm B} = \frac{1 \times 8}{6} = 1.333 \, \rm kN$$

 $R_{\rm A} = 0.333 \, \rm kN \downarrow$

• Taking sagging moment as positive and hogging moment as negative, find out the expressions for moments in various portions of the beam due to external loading and unit force where the deflection is to be determined in a Tabular form.



Q2. Determine the deflection and rotation at the free end of the cantilever beam shown in Figure by unit load method. Given $E = 200000 \text{ N/mm}^2$ and $I = 12 \times 10^6 \text{ mm}^4$



• Find out the deflection and rotation at the free end of the cantilever beam, apply unit load for deflection and unit moment for rotation at the free end of the beam as shown in Figure.

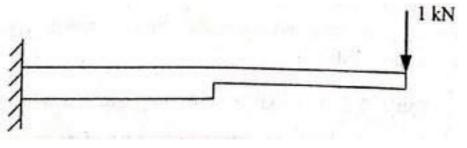


Figure 1: Beam with unit vertical load at 'C'

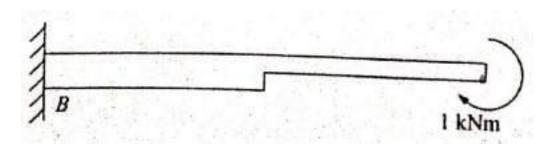


Figure 2: Beam with unit moment at 'C'

- The bending moment expressions can be calculated by
- *M* for external given load, m_1 for unit vertical load at 'C' and m_2 for unit moment at 'C' for various portion of cantilever beam and tabulated below.

Portion	CB	ВА
Origin	С	В
Limit	0 - 2	0 - 2
М	-20x	-[20(2+x)+20x]
<i>m</i> ₁	x	-(x + 2)
<i>m</i> ₂	-1	-1
I	I _o	2 <i>I</i> _o

Vertical deflection at
$$C = \Delta = \int_{0}^{L} \frac{Mm_{1}}{EI} dx$$

$$= \int_{0}^{2} \frac{(-20x)(-x)}{EI_{0}} dx + \int_{0}^{2} \frac{[20(2+x)+20x](x+2)}{E2I_{0}} dx$$

$$= \int_{0}^{2} \frac{20x^{2}}{EI_{0}} dx + \int_{0}^{2} \frac{(40x+40)(x+2)}{2EI_{0}} dx$$

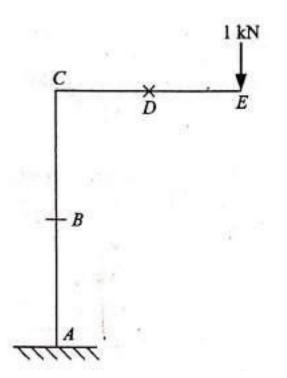
$$= \left[\frac{20}{3} \frac{x^{3}}{EI_{0}}\right]_{0}^{2} + \frac{1}{2EI_{0}} \left[\frac{40x^{3}}{3} + \frac{120x^{2}}{2} + 80x\right]_{0}^{2}$$

$$= \frac{53.333}{EI_{0}} + \frac{1}{EI_{0}} [253.333]$$

$$= \frac{306.67}{EI_{0}}$$

Rotation at 'C' = $\theta_c = \int_0^L \frac{Mm_2}{EI} = \int_0^2 \frac{(20x)}{EI_0} dx + \int_0^2 \frac{(40x+40)1}{E2I_0} dx$ $\left[\frac{20}{EI_o}\frac{x^2}{2}\right]_0^2 + \frac{1}{EI_o}\left[\frac{40x^2}{2}\right]$ +40x160 40 EI 120 EI.

Q3. Determine the vertical and horizontal deflection at the free end of the bent shown in Figure by unit load method. Assume uniform flexural rigidity *EI* throughout.



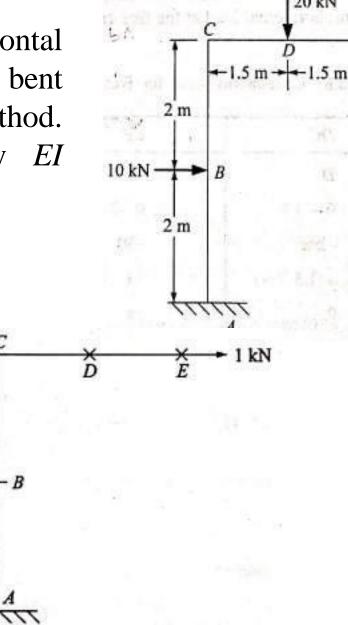


Figure 1: Frame with unit vertical load at 'E'

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Figure 2: Frame with unit horizontal load at 'E'

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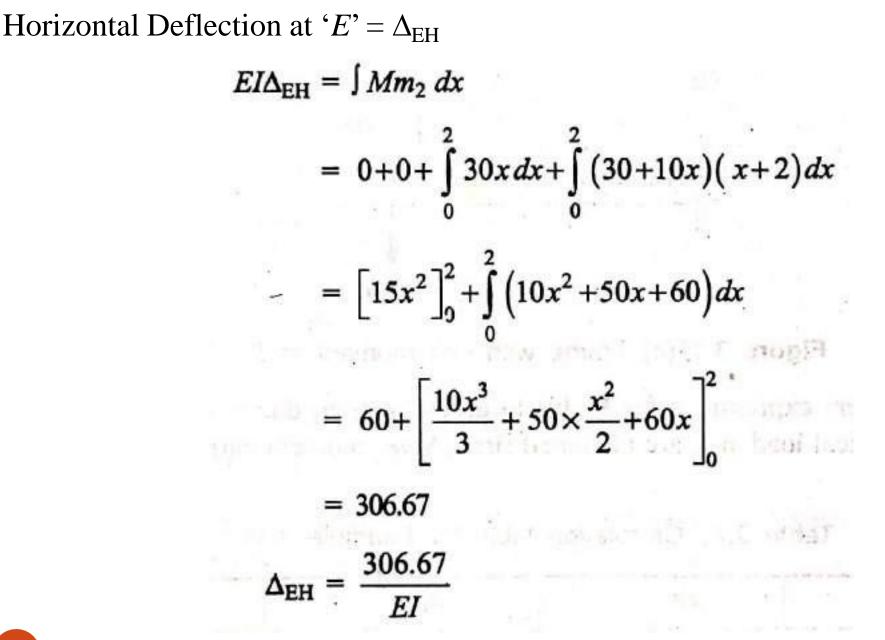
• Find out the expressions in Tabular form for moment 'M' due to external loads, m_1 due to the unit vertical load present at the free end (Figure 1) and m_2 due to the unit horizontal load present at the free end (Figure 2) of the bent.

Portion	ED	DC	CB	BA
Origin	E	D	C	В
Limit	0 - 1.5	0 - 1.5	0 -2	0 - 2
M	0	-20x	-30	-30 -10x
<i>m</i> ₁	, x	-(1.5 + x)	-3	-3
<i>m</i> ₂	0	0	-x	-(x+2)
Flexural Rigidity	EI	EI	El	EI

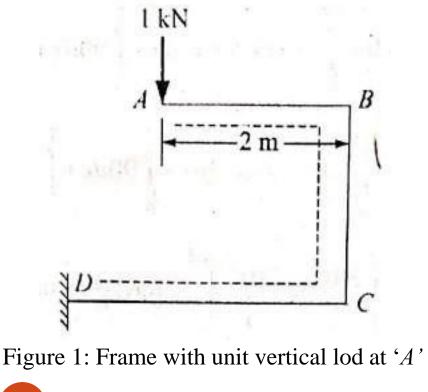
Note: Moment carrying tension on dotted side is taken as positive

Vertical deflection at ' $E' = \Delta_{EV}$

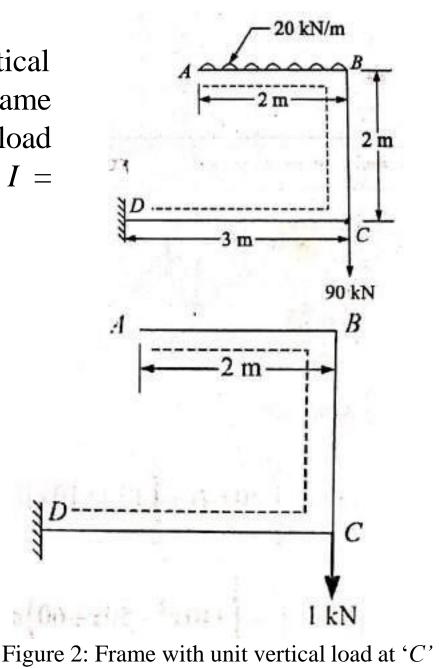
$$\begin{split} EI\Delta_{\rm EV} &= \int Mm_1 \, dx \\ &= 0 + \int_0^{1.5} 20x(1.5+x) \, dx + \int_0^2 90 \, dx + \int_0^2 (90+30x) \, dx \\ &= \int_0^{1.5} (30x+20x^2) \, dx + \int_0^2 90 \, dx + \int_0^2 (90+30x) \, dx \\ &= \left[\frac{30x^2}{2} + \frac{20x^3}{3} \right]_0^{1.5} + [90x]_0^2 + \left[90x + \frac{30x^2}{2} \right]_0^2 \\ &= 56.25 + 180 + 240 \\ &= 476.25 \\ \Delta_{\rm EV} &= \frac{476.25}{EI} \end{split}$$



Q4. Determine the vertical deflections at A and C in the frame shown in Figure by unit load method. Take E = 200 GPa, $I = 150 \times 10^4$ mm⁴.



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• The bending moment expressions for 'M' due to given load, m_1 due to unit vertical load at A and m_2 due to unit vertical load at C are Tabulated below.

	Portion	AB	BC	CD
tols" (n)	Origin for ment- in	and A million &	B	Card Prinkers
	Limit	0 - 2	0 - 2	0 -3
	М	10x ²	40	40 -130x
m_I	m _I	x	2	2 - x
	<i>m</i> ₂	0	0	
Flexural Rigidity	Flexural Rigidity	EI	EI	-1

Vertical deflection at $A = \Delta_A$

$$EI\Delta_{\Lambda} = \int_{0}^{2} 10x^{2} \cdot x dx + \int_{0}^{2} 80 dx + \int_{0}^{3} (40 - 130x)(2 - x) dx$$
$$= \left[\frac{10x^{4}}{4}\right]_{0}^{2} + \left[80x\right]_{0}^{2} + \int_{0}^{3} (80 - 300x + 130x^{2}) dx$$

$$= \frac{10(2^{4})}{4} + 80(2) + \left[80x - 300\frac{x^{2}}{2} + \frac{130x^{3}}{3} \right]_{0}^{3}$$

$$= 260$$

 $E = 240 \text{ GPa} = 240 \times 10^{9} \text{ N/m}^{2}$
 $I = 150 \times 10^{4} \text{ mm}^{4} = 150 \times 10^{4} \times 10^{-12} \text{ m}^{4}$

$$= 150 \times 10^{-8} \text{ m}^{4}$$

$$\therefore \Delta = \frac{260}{240 \times 10^{9} \times 150 \times 10^{-8}} = 7.222 \times 10^{-4} \text{ m}$$

$$= 0.722 \text{ mm}$$

Vertical Deflection at $C = \Delta_c$

$$EI\Delta_{c} = \int Mm_{2} dx$$

= $0 + 0 + \int_{0}^{3} (40 - 130x)(-x) dx$
= $\int_{0}^{3} (-40x + 130x^{2}) dx$
= $\left[-20x^{2} + 130\frac{x^{3}}{3} \right]_{0}^{3}$
= 990
 $\Delta_{c} = \frac{990}{240 \times 10^{9} \times 150 \times 10^{-8}} = 2.75 \times 10^{-3} \text{ m}$
= 2.75 mm

Thanks