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AN AUTONOMOUS INSTITUTION

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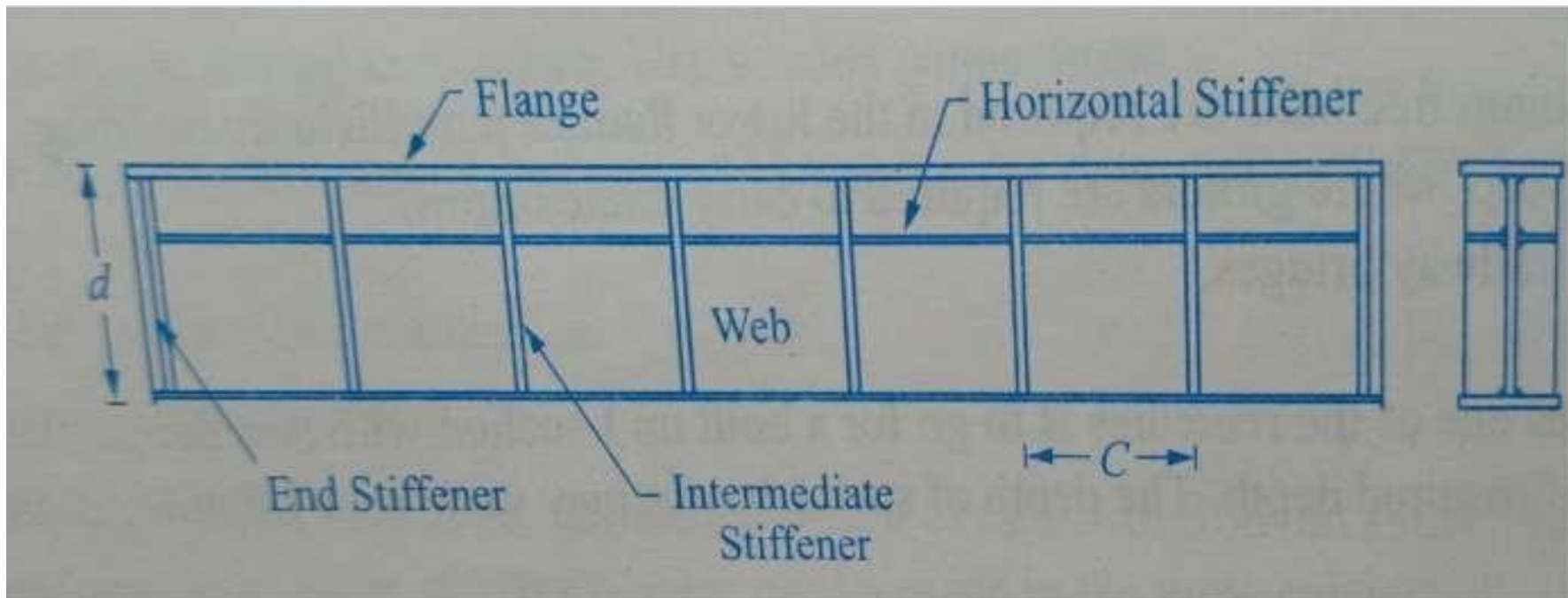


DEPARTMENT OF CIVIL ENGINEERING

19CET304-DESIGN OF STEEL STRUCTURES

III YEAR / VI SEMESTER

Unit 5 :DESIGN OF PLATE GIRDERS, GANTRY GIRDERS & ROOF TRUSSES Topic – Design of Welded Plate girder



- A plate girder is a beam built up from plate elements to achieve a more efficient arrangement of material than is possible with rolled beams.
- Plate girders are economical where the spans are long enough to permit saving in cost by proportioning for the particular requirements.
- Plate girders may be of riveted, bolted, or welded constructions.

ELEMENTS OF PLATE GIRDER

1. WEB
2. FLANGE
3. STIFFENERS

Webs of required depth and thickness are provided to

- a) Keep flange plates at required distances.
- b) Resist the shear in beam.

Flanges of required width and thickness are provided to resist bending moment developing compressive force in one flange and tensile force in another flange.

Stiffeners are provided to safeguard the web against local buckling. Stiffeners are provided along transverse(vertical) and longitudinal(Horizontal) direction.

Transverse Stiffeners are of two types.

- A) End Bearing Stiffeners and B) intermediate stiffeners

A) End Bearing Stiffeners-These are provided to transfer the load from beam to support. Near the support, certain portion of web is subjected to compression, so there is possibility of crushing of web. Web needs some stiffeners to transfer load to support.

B)Intermediate stiffeners: To resist shear, the required thickness of web may be very small. As thickness is small. To avoid buckling, intermediate stiffeners may be required.

Design a welded plate girder of span 24 m to carry a super imposed load 35 kN/m. Avoid using of bearing and intermediate stiffeners. Use Fe415 steel.

Solution:

1. Calculation of moment and shear Force:

Span=24 m, Super imposed load= 35 kN/m,

Factored super imposed load= $35 \times 1.5 = 52.5$ kN/m

Total factored super imposed load= $1.5 \times 35 \times 24 = 1260$ kN

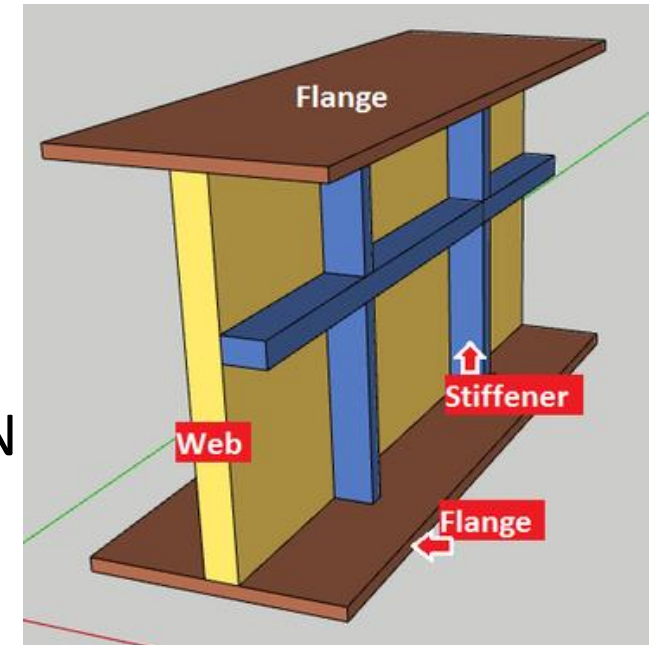
Self weight= $1260/200 = 6.3$ kN/m

Total load= $52.5 + 6.3 = 58.8$ kN/m

Bending moment= $58.8 \times 24^2/8$

=4233.6 kNm

SF= $58.8 \times 24/2 = 705.6$ kN



2. Depth of web Plate

Avoiding stiffeners, $d/t_w \leq 67$

Economical depth of web

$$d = [Mk/f_y]^{1/3}$$

$$D = \{4233.6 * 103 * 67 / 250\}^{1/3} = 1043 \text{ mm}$$

Taking 1000 mm plate $t_w \geq [1000/67 = 14.92 \text{ mm}]$ Take $t_w = 16 \text{ mm}$

Web plate is 1000 mm * 16 mm

3. Selection of Flange:

Assuming moment to be taken by flange

alone $[A_f \cdot f_y \cdot d / 1.1] \geq M$

$$A_f \geq M \cdot 1.1 / [f_y \cdot d]$$

$$A_f \geq [4233.6 \cdot 106 \cdot 1.1 / \{250 \cdot 1000\}] \geq 18628 \text{ mm}^2$$

For making it a plastic section $b/t_f \leq 8.4$

$$b_f / (2 \cdot t_f) \leq 8.4$$

$$b_f = 16.8 t_f$$

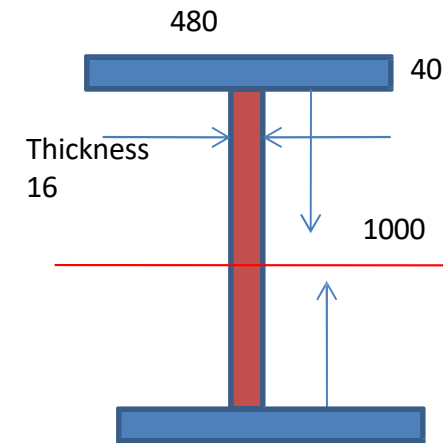
$$A_f = b_f \cdot t_f = 16.8 t_f \cdot t_f \geq 18628 \text{ mm}^2$$

which gives $t_f = 33.3 \text{ mm}$

Taking 40 mm thick plate ,

$$b_f = 18628 / 40 = 465.7 \text{ mm}$$

Use flange plate=480 mm*40 mm.

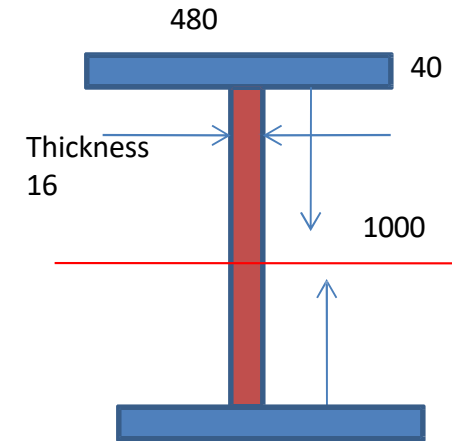


4. Checking Moment Capacity of Girder

$$M_d = [Z_p \cdot f_y / 1.1] \leq 1.2 \cdot Z_e \cdot f_y / 1.1$$

$$M_d = [Z_p \cdot f_y / 1.1] = [480 \cdot 40 \cdot (1000 + 40/2 + 40/2) \cdot 250 / 1.1] \\ = 4538.182 \text{ kN} \leq 1.2 \cdot Z_e \cdot f_y / 1.1$$

$$I_{zz} = 2 \cdot \left[\frac{1}{12} \cdot 480 \cdot 40^3 + 480 \cdot 40 \cdot \left(\frac{1000 + 40}{2} \right)^2 \right] = 1.2 \cdot Z_e \cdot \frac{f_y}{1.1} = 1.2 \cdot [I_{zz} / y_{max}] \cdot 250 / 1.1 == \\ = 2 \cdot 5601.28 \cdot 10^6 \text{ mm}^4 \quad = 1.2 \cdot [2 \cdot 5601.28 \cdot 10^6 / 540] \cdot 250 / 1.1 == \\ = 5657.82 \text{ kNm}$$



$$M_d = 4538.182 > [M = 4233.6 \text{ kNm}]$$

5. Shear Resisting Capacity:

$$V_d = \frac{A_v * f_{yw}}{1.1 * \sqrt{3}} = \frac{d * t_w * f_{yw}}{1.1 * \sqrt{3}} = \frac{1000 * 16 * 250}{1.1 * \sqrt{3}} \\ = 2099.45 \text{ kN} > 705.6 \text{ kN}$$

No stiffener is required.

6. Check for End Bearing:

Bearing strength of web: $F_w = (b_1 + n_2) t_w * f_{yw} / 1.1$

Assuming width of bearing 200 mm and stiff bearing length 100 mm

$$n_2 = 2.5 * b_f = 2.5 * 40 = 100 \text{ mm}$$

$$F_w = (100 + 100) 16 * 250 / 1.1 = 727 \text{ kN} > 705.6 \text{ kN}$$

So, safe.

7.Weld Design to join web to Flange:

Shear force=705.6 kN

Shear force per mm length in the junction= $0.512 \times 480 = 245.76$ N

If s is the size of the weld, providing weld on both sides

$$2 * 0.7 * s * \frac{410}{\sqrt{3} * 1.25} = 265.1 s = 245.76, s = 0.92 \text{ mm}$$

As minimum weld thickness is 5 mm for web thickness 16 mm, so provide intermittent welds.

Percentage of weld= $0.92 \times 100 / 5 = 18.4$ %,

Taking 20% weld length

As minimum weld length 40 mm, unweld length will be $40 \times 4 = 160$ mm

Maximum unweld length= $12 \times t = 12 \times 16 = 192 > 160$ so OK>



Thank you